Corrosion Behaviour of AGR Simulated Fuels – Evolution of the Fuel Surface

<u>Nadya Rauff-Nisthar¹</u>, Colin Boxall¹, Ian Farnan², Zoltan Hiezl³, William Lee³, Chris Perkins⁴ and Richard Wilbraham¹

¹Lancaster University, Engineering Department, LA1 4YR, UK, ²University of Cambridge, Department of Earth Sciences, CB2 3EQ, UK, ³Imperial College London, Department of Materials, SW7 2BP, UK, ⁴National Nuclear Laboratory, Preston Laboratory, A709, Springfields, Salwick, PR4 0XJ

The vast proportion of spent fuel in the UK comes from Advanced Gas-Cooled Reactors (AGR). Current UK nuclear waste policy is that spent AGR fuel is to be contained in steel canisters and disposed of directly via burial in a geological repository. It is expected that after 1000 years, once the thermal pulse has occurred, that the steel canisters in which spent AGR fuel pellets are stored in will come into contact with groundwater, corrode, and subsequently fail. The failure of these steel canisters will lead to the corrosion of the spent uranium dioxide fuel inside the canister under environmental conditions. Alpha radiation is the only type of radiation that is expected to prevail after the thermal pulse. However, when groundwater comes into contact with alpha radiation produced by UO₂ fuel pellets, alpha radiolysis of water will take place, resulting in the formation of oxidising species such as hydroxyl radicals and hydrogen peroxide.

When H_2O_2 reacts with UO_2 under groundwater conditions, secondary uranyl peroxide mineral phases are produced, in particular studites and metastudites, on the surface of UO_2 . The stability of these minerals has not hitherto been studied on UK specific spent fuel, especially in the presence of high carbonate concentrations, which are expected to be present in UK repository groundwater compositions. Thus, it is currently unknown whether the presence of uranyl peroxides will retard the migration of radionuclides from the spent fuel matrix.

Here we present for the first time

electrochemical/alpha spectroscopy experiments into the effect of deliberately added H_2O_2 on electrodeposited uranium oxide steel planchets acting as simple model fuel pin assemblies. At $[H_2O_2] \le 100 \mu \text{mol dm}^{-3}$, dissolution of the electrodeposited uranium oxide surface proceeds rapidly, unimpeded by any corrosion product layer. At H_2O_2 concentrations between 1 and 100 mmol dm⁻³ the electrodeposited film is covered by a studtite corrosion product layer and uranium oxide dissolution is slow. Finally, at a H_2O_2 concentration > 100 mmol dm⁻³ the uranium oxide film again begins to dissolve, uninhibited by the presence of a corrosion product layer. Such corrosion processes have been described through the formation of a novel pseudo-polargram, Figure 1.

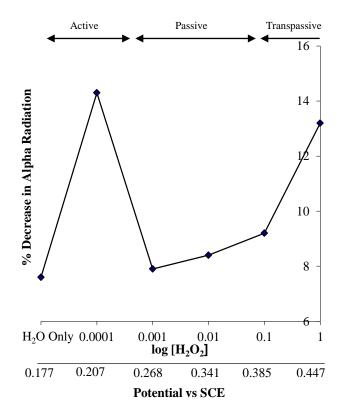


Figure 1- Pseudo current vs. potential plot showing the effect of hydrogen peroxide concentration on a electrodeposited uranium oxide planchet in pH 6.1 distilled water

We also discuss here preliminary cyclic voltammetric and impedance spectroscopy results for more realistic SimFuel rotating disc electrode (RDE) samples in increasing H_2O_2 concentrations. Future experiments will aim to measure SimFuel RDE corrosion rates under equivalent UK repository groundwater conditions.