Corrosion Resistance of Oxide Scales Formed in High-Temperature Oxidation of Al-Bearing Ferritic Stainless Steels

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Al-bearing ferritic stainless steels with the oxide scales formed in a high temperature oxidation are used as a support material of a catalytic converter in vehicles. Aqueous condensates are produced in the exhaust system during the short-distance driving. The condensates cause localized corrosion of the stainless steel components. In this study, the corrosion resistance of the oxide scales on Al-bearing ferritic stainless steels under the aqueous condensate environment was investigated.

Two kinds of ferritic stainless steel foils (Fe-20Cr-5Al, Fe-20Cr-8Al), which were 32 μ m in thickness, were used as specimens. All the specimens were heat-treated at 973, 1173, and 1373 K for 1 h in air to form oxide scales on the surface. Electrochemical measurements were conducted in the condensate at 363 K simulating the exhaust system of vehicles. The ionic composition of the simulated condensate is shown in Table 1.The condensate was adjusted to pH 3.5 using a H₂SO₄ solution.

Figure 1 shows the cathodic polarization curves of Fe-20Cr-5Al and Fe-20Cr-8Al oxidized at temperatures $(T_{\rm ox})$ of 973, 1173, and 1373 K. Cathodic reactions were inhibited with the increase of $T_{\rm ox}$ and the additive amount of Al. The polarization curve in a phosphate buffer solution (pH = 3.5) in Fig. 2 reveals that the cathodic behaviors of the oxide scales are not affected by the ionic composition of the condensate.

Figure 3 indicates the depth profiles of cation fractions for the oxide scales of Fe-20Cr-5Al and Fe-20Cr-8Al measured by GD-OES. In this study, just the cation fractions of Fe, Cr, and Al $(X_{\text{Fe}}, X_{\text{Cr}}, \text{ and } X_{\text{Al}})$ were taken into account; $X_{\text{Fe}} + X_{\text{Cr}} + X_{\text{Al}} = 1$. Thickness of the oxide layer was calculated on the basis of oxygen profiles by GD-OES. In the case of Fe-20Cr-5Al oxidized at 973 and 1173 K, Fe-rich oxide was formed in the outermost layer of the scall. This result indicates the cathode current detected in Fig. 1 was caused by the reductive dissolution of Fe₂O₃. The depth profiles of the cation fractions for Fe-20Cr-5Al oxidized at 973 K after the potentiostatic polarization at -0.1 V vs. Ag/AgCl (3.33 M KCl) in the codensate at 363 K are shown in Fig. 4. It is confirmed that the thickness of the oxide layer decreased, and the Ferich outer layer disappeared in comparison with Fig. 3a. Figure 4 certainly supports the reductive dissolution of Fe oxides. Figure 3c and 3d suggest that the increases of T_{ox} and the additive amount of Al brought the growth of Alrich oxide layers instead of Fe-rich ones. The inhibition of cathodic reactions shown in Fig. 1 corresponds to the form of the inert Al-rich oxide layer. It is expected that the oxide scales formed by the high-temperature oxidation of Fe-20Cr-8Al have high corrosion resistance.

Table 1 Ionic composition of the simulated condensate.



Fig. 1 Cathodic polarization curves of (a) Fe-20Cr-5Al oxidized at 973, 1173, and 1373 K, and (b) Fe-20Cr-5Al and -8Al oxidized at 1173 K in the simulated condensate.



Fig. 2 Cathodic polarization curves of Fe-20Cr-5Al oxidized at 973 K in the simulated condensate and a phosphate buffer solution at 363 K.



Fig. 3 Depth profiles of cation fractions for the oxide scales of (a) Fe-20Cr-5Al oxidized at 973 K, (b) 1173 K, and (c) 1373 K, and (d) Fe-20Cr-8Al oxidized at 1173 K.



Fig. 4 Depth profiles of cation fractions for the oxide scales of Fe-20Cr-5Al oxidized at 973 K after the potentiostatic polarization at -0.1 V for 50 min.